



## OPAx348-Q1 1-MHz 45- $\mu$ A CMOS Rail-to-Rail Operational Amplifier

### 1 Features

- Qualified for Automotive Applications
- AEC-Q100 Qualified With the Following Results:
  - Device Temperature Grade 1:  $-40^{\circ}\text{C}$  to  $+125^{\circ}\text{C}$  Ambient Operating Temperature Range
  - Device HBM ESD Classification Level 2
  - Device CDM ESD Classification Level C4B
- Low Quiescent Current ( $I_Q$ ): 45  $\mu\text{A}$  (Typ)
- Low Cost
- Rail-to-Rail Input and Output
- Single Supply: 2.1 V to 5.5 V
- Input Bias Current: 0.5 pA (Typ)
- High Speed: Power With Bandwidth: 1 MHz

### 2 Applications

- Portable Equipment
- Battery-Powered Equipment
- Smoke Alarms
- CO Detectors
- HEV/EV and Power Train
- Infotainment and Cluster
- Medical Instrumentation

### 3 Description

The OPAx348-Q1 series of devices are single-supply, low-power CMOS operational amplifiers. Featuring an extended bandwidth of 1 MHz and a supply current of 45  $\mu\text{A}$ , the OPAx348-Q1 family of devices is useful for low-power applications on single supplies of 2.1 V to 5.5 V.

Low supply current of 45  $\mu\text{A}$  and an input bias current of 0.5 pA make the OPAx348-Q1 family of devices an optimal candidate for low-power, high-impedance applications such as smoke detectors and other sensors.

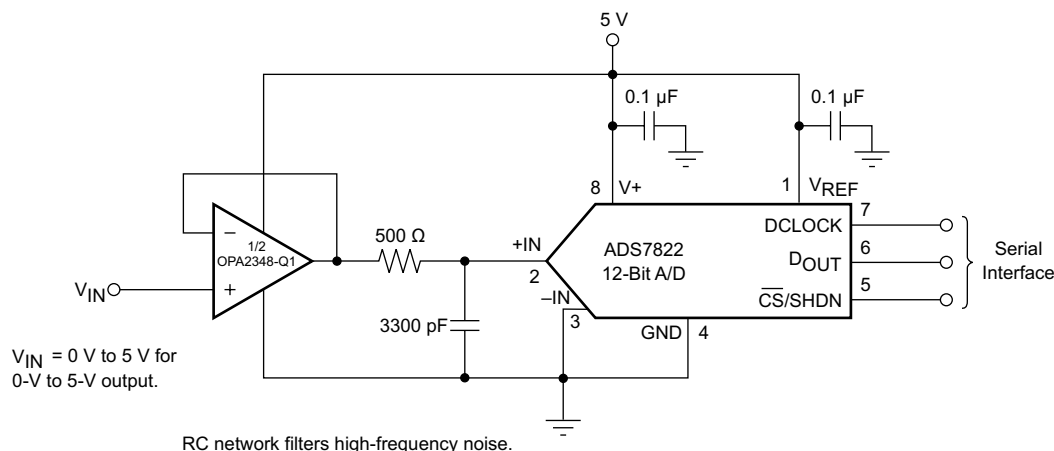
The OPA348-Q1 device is available in both the SOT23-5 (DBV) and the SOIC (D) packages. The OPA2348-Q1 device is available in the SOIC-8 (D) package. The OPA4348-Q1 device is available in the TSSOP-14 (PW) package. The automotive temperature range of  $-40^{\circ}\text{C}$  to  $+125^{\circ}\text{C}$  over all supply voltages offers additional design flexibility.

#### Device Information<sup>(1)</sup>

PART NUMBER	PACKAGE	BODY SIZE (NOM)
OPA348-Q1	SOT-23 (5)	2.90 mm $\times$ 1.60 mm
	SOIC (8)	4.90 mm $\times$ 3.91 mm
OPA2348-Q1	SOIC (8)	4.90 mm $\times$ 3.91 mm
OPA4348-Q1	TSSOP (14)	5.00 mm $\times$ 4.40 mm

(1) For all available packages, see the orderable addendum at the end of the datasheet.

#### Noninverting Configuration Driving ADS7822



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## 4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

### Changes from Revision B (December 2014) to Revision C Page

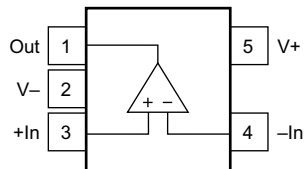
- Added the OPA348-Q1 SOIC (D) package option to document ..... **1**

### Changes from Revision A (January 2009) to Revision B Page

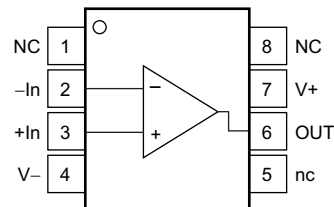
- Added two new applications to the *Applications* section ..... **1**
- Added the *ESD Ratings* table, *Feature Description* section, *Device Functional Modes* section, *Application and Implementation* section, *Power Supply Recommendations* section, *Layout* section, *Device and Documentation Support* section, and *Mechanical, Packaging, and Orderable Information* section ..... **1**
- Added the OPA348-Q1 device to the data sheet ..... **1**
- Changed the name for pin 3 in the PW (TSSOP) package drawing ..... **4**

## 5 Pin Configuration and Functions

**DBV Package: OPA348-Q1**  
**5-Pin SOT-23**  
**Top View**



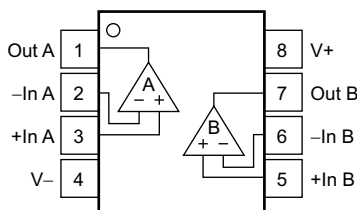
**D Package: OPA348-Q1**  
**8-Pin SOIC**  
**Top View**



**Pin Functions: OPA348-Q1**

NAME	PIN NO.		I/O	DESCRIPTION
	SOT-23	SOIC		
+IN	3	3	I	Noninverting input
-IN	4	2	I	Inverting input
OUT	1	6	O	Output
V+	5	7	—	Positive (highest) supply
V-	2	4	—	Negative (lowest) supply
NC	—	1	—	Do not connect
		5		
		8		

**D Package: OPA2348-Q1**  
**8-Pin SOIC**  
**Top View**



**Pin Functions: OPA2348-Q1**

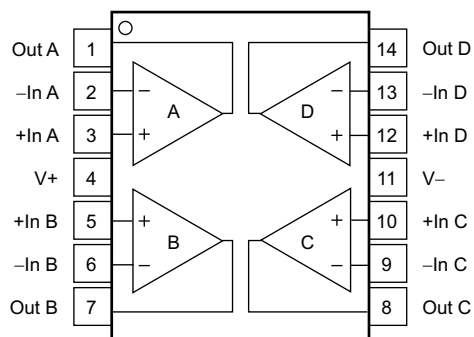
NAME	PIN NO.		I/O	DESCRIPTION
+IN A	3		I	Noninverting input, Channel A
-IN A	2		I	Inverting input, Channel A
+IN B	5		I	Noninverting input, Channel B
-IN B	6		I	Inverting input, Channel B
OUT A	1		O	Output, Channel A
OUT B	7		O	Output, Channel B
V+	8		—	Positive (highest) supply
V-	4		—	Negative (lowest) supply

**OPA348-Q1, OPA2348-Q1, OPA4348-Q1**

SBOS465C – JANUARY 2009 – REVISED JANUARY 2016

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**PW Package: OPA4348-Q1**  
**14-Pin TSSOP**  
**Top View**



**Pin Functions: OPA4348-Q1**

PIN		I/O	DESCRIPTION
NAME	NO.		
+IN A	3	I	Noninverting input, Channel A
–IN A	2	I	Inverting input, Channel A
+IN B	5	I	Noninverting input, Channel B
–IN B	6	I	Inverting input, Channel B
+IN C	10	I	Noninverting input, Channel C
–IN C	9	I	Inverting input, Channel C
+IN D	12	I	Noninverting input, Channel D
–IN D	13	I	Inverting input, Channel D
OUT A	1	O	Output, Channel A
OUT B	7	O	Output, Channel B
OUT C	8	O	Output, Channel C
OUT D	14	O	Output, Channel D
V+	4	—	Positive (highest) supply
V–	11	—	Negative (lowest) supply

## 6 Specifications

### 6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

		MIN	MAX	UNIT
Supply voltage, $V_S$	$V_-$ to $V_+$		7.5	V
Input voltage, $V_{IN}$	Signal input terminals <sup>(2)</sup>	$(V_-) - 0.5\text{ V}$	$(V_+) + 0.5\text{ V}$	V
Input current, $I_{IN}$	Signal input terminals <sup>(2)</sup>		10	mA
Output short-circuit duration <sup>(3)</sup>		Continuous		
Operating free-air temperature, $T_A$		-40	150	°C
Operating virtual-junction temperature, $T_J$			150	°C
Storage temperature, $T_{sig}$		-65	150	°C

- (1) Stresses beyond those listed under *absolute maximum ratings* may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under *recommended operating conditions* is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) Input terminals are diode-clamped to the power-supply rails. Input signals that can swing more than 0.5 V beyond the supply rails should be current-limited to 10 mA or less.
- (3) Short-circuit to ground, one amplifier per package.

### 6.2 ESD Ratings

		VALUE	UNIT
$V_{(ESD)}$ Electrostatic discharge	Human-body model (HBM), per AEC Q100-002 <sup>(1)</sup>	±2000	V
	Charged-device model (CDM), per AEC Q100-011	±500	
	Corner pins (1, 7, 8, and 14)	±750	

- (1) AEC Q100-002 indicates that HBM stressing shall be in accordance with the ANSI/ESDA/JEDEC JS-001 specification.

### 6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	MAX	UNIT
$V_S$	Supply voltage, $V_-$ to $V_+$	2.1	5.5	V
$T_A$	Operating free-air temperature	-40	125	°C

## 6.4 Thermal Information: OPA348-Q1

THERMAL METRIC <sup>(1)</sup>		OPA348-Q1		UNIT
		DBV (SOT-23)	D (SOIC)	
		5 PINS	8 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	228.5	142.0	°C/W
$R_{\theta JC(top)}$	Junction-to-case (top) thermal resistance	99.1	90.2	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	54.6	82.5	°C/W
$\Psi_{JT}$	Junction-to-top characterization parameter	7.7	39.4	°C/W
$\Psi_{JB}$	Junction-to-board characterization parameter	53.8	82.0	°C/W
$R_{\theta JC(bottom)}$	Junction-to-case (bottom) thermal resistance	n/a	n/a	°C/W

- (1) For more information about traditional and new thermal metrics, see the *Semiconductor and IC Package Thermal Metrics* application report, [SPRA953](#).

## 6.5 Thermal Information: OPA2348-Q1, OPA4348-Q1

THERMAL METRIC <sup>(1)</sup>		OPA2348-Q1	OPA4348-Q1	UNIT
		D (SOIC)	PW (TSSOP)	
		8 PINS	14 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	138.4	121	°C/W
$R_{\theta JC(top)}$	Junction-to-case (top) thermal resistance	89.5	49.4	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	78.6	62.8	°C/W
$\Psi_{JT}$	Junction-to-top characterization parameter	29.9	5.9	°C/W
$\Psi_{JB}$	Junction-to-board characterization parameter	78.1	62.2	°C/W
$R_{\theta JC(bottom)}$	Junction-to-case (bottom) thermal resistance	n/a	n/a	°C/W

- (1) For more information about traditional and new thermal metrics, see the *Semiconductor and IC Package Thermal Metrics* application report, [SPRA953](#).

## 6.6 Electrical Characteristics

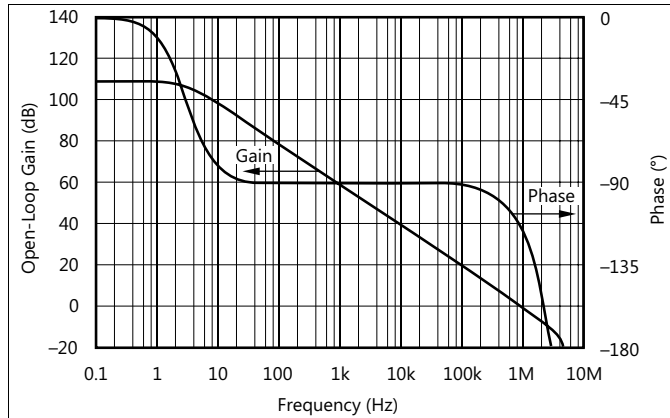
At  $V_S = 2.5\text{ V}$  to  $5.5\text{ V}$ ,  $R_L = 100\text{ k}\Omega$  connected to  $V_S / 2$ ,  $V_{OUT} = V_S / 2$  (unless otherwise noted).

PARAMETER		TEST CONDITIONS	$T_A^{(1)}$	MIN	TYP	MAX	UNIT
$V_{OS}$	Input offset voltage	$V_S = 5\text{ V}$ , $V_{CM} = (V-) + 0.8\text{ V}$	25°C		1	5	mV
			Full range			6	
$\Delta V_{OS}/\Delta T$	Offset voltage drift over temperature		Full range		4		$\mu\text{V}/^\circ\text{C}$
PSRR	Offset voltage drift vs power supply	$V_S = 2.5\text{ V}$ to $5.5\text{ V}$ , $V_{CM} < (V+) - 1.7\text{ V}$	25°C		60	175	$\mu\text{V}/\text{V}$
			Full range			300	
	Channel separation	dc	25°C		0.2		$\mu\text{V}/\text{V}$
		$f = 1\text{ kHz}$	25°C		134		dB
$V_{CM}$	Input common-mode voltage range		25°C	$(V-) - 0.2$		$(V+) + 0.2$	V
CMRR	Input common-mode rejection ratio	$(V-) - 0.2\text{ V} < V_{CM} < (V+) - 1.7\text{ V}$	25°C		70	82	dB
			Full range			66	
		$V_S = 5.5\text{ V}$ , $(V-) - 0.2\text{ V} < V_{CM} < (V+) + 0.2\text{ V}$	25°C		60	71	
			Full range			56	
$I_B$	Input bias current		25°C		$\pm 0.5$	$\pm 10$	pA
$I_{OS}$	Input offset current		25°C		$\pm 0.5$	$\pm 10$	pA
$Z_i$	Input impedance	Differential	25°C		$10^{13} \parallel 3$		$\Omega \parallel \text{pF}$
		Common-mode			$10^{13} \parallel 3$		
	Input voltage noise	$V_{CM} < (V+) - 1.7\text{ V}$ , $f = 0.1\text{ Hz}$ to $10\text{ Hz}$	25°C		10		$\mu\text{V}_{PP}$
$V_n$	Input voltage noise density	$V_{CM} < (V+) - 1.7\text{ V}$ , $f = 1\text{ kHz}$	25°C		35		$\text{nV}/\sqrt{\text{Hz}}$
$I_n$	Input current noise density	$V_{CM} < (V+) - 1.7\text{ V}$ , $f = 1\text{ kHz}$	25°C		4		$\text{fA}/\sqrt{\text{Hz}}$
$A_{OL}$	Open-loop voltage gain	$V_S = 5\text{ V}$ , $R_L = 100\text{ k}\Omega$ , $0.025\text{ V} < V_O < 4.975\text{ V}$	25°C		94	108	dB
			Full range			90	
		$V_S = 5\text{ V}$ , $R_L = 5\text{ k}\Omega$ , $0.125\text{ V} < V_O < 4.875\text{ V}$	25°C		90	98	
			Full range			88	
	Voltage output swing from rail	$R_L = 100\text{ k}\Omega$ , $A_{OL} > 94\text{ dB}$	25°C		18	25	mV
			Full range			25	
		$R_L = 5\text{ k}\Omega$ , $A_{OL} > 90\text{ dB}$	25°C		100	125	mV
			Full range			125	
$I_{SC}$	Output short-circuit current		25°C		$\pm 10$		mA
$C_{LOAD}$	Capacitive load drive	See the <a href="#">Typical Characteristics</a> section	25°C				
GBW	Gain-bandwidth product	$C_L = 100\text{ pF}$	25°C		1		MHz
SR	Slew rate	$C_L = 100\text{ pF}$ , $G = +1$	25°C		0.5		V/ $\mu\text{s}$
$t_s$	Settling time	$C_L = 100\text{ pF}$ , $V_S = 5.5\text{ V}$ , 2V- step, $G = +1$	25°C		5		$\mu\text{s}$
					7		
	Overload recovery time	$V_{IN} \times \text{Gain} > V_S$	25°C		1.6		$\mu\text{s}$
THD+N	Total harmonic distortion plus noise	$C_L = 100\text{ pF}$ , $V_S = 5.5\text{ V}$ , $V_O = 3\text{ V}_{PP}$ , $G = +1$ , $f = 1\text{ kHz}$	25°C		0.0023%		
$I_Q$	Quiescent current	Per amplifier	25°C		45	65	$\mu\text{A}$
			Full range			75	

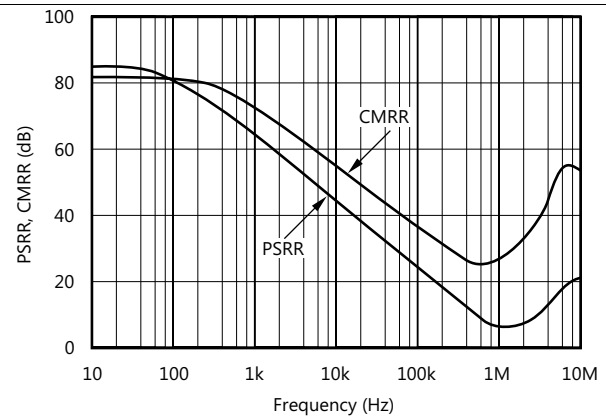
(1) Full range  $T_A = -40^\circ\text{C}$  to  $+125^\circ\text{C}$ .

## 6.7 Typical Characteristics

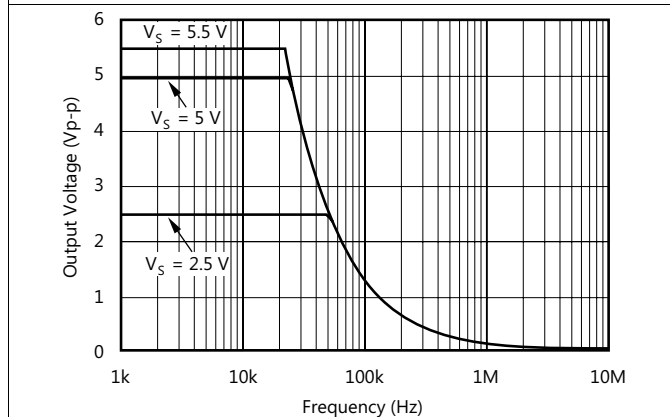
At  $T_A = 25^\circ\text{C}$ ,  $R_L = 100\text{ k}\Omega$  connected to  $V_S / 2$ ,  $V_{OUT} = V_S / 2$  (unless otherwise noted).



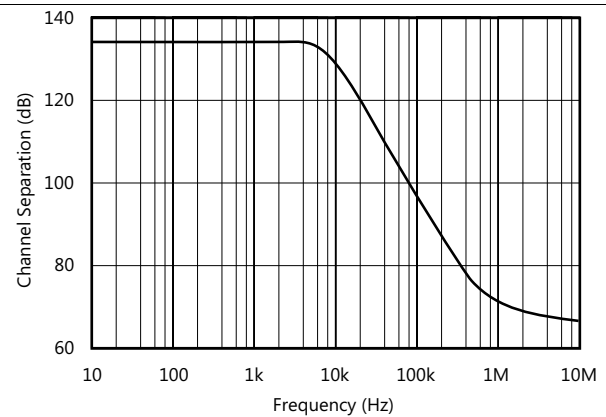
**Figure 1. Open-Loop Gain and Phase vs Frequency**



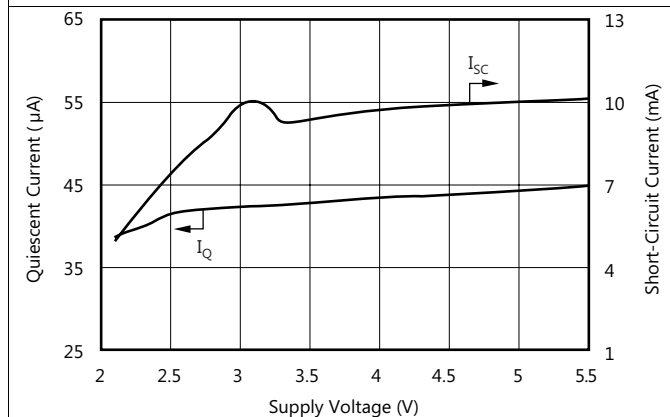
**Figure 2. PSRR and CMRR vs Frequency**



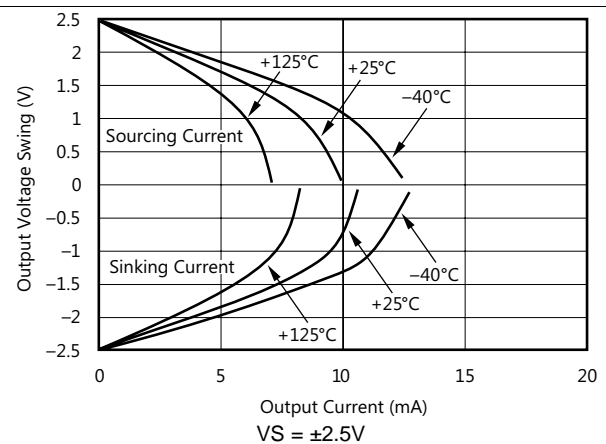
**Figure 3. Maximum Output Voltage vs Frequency**



**Figure 4. Channel Separation vs Frequency**



**Figure 5. Quiescent and Short-Circuit Current vs Supply Voltage**

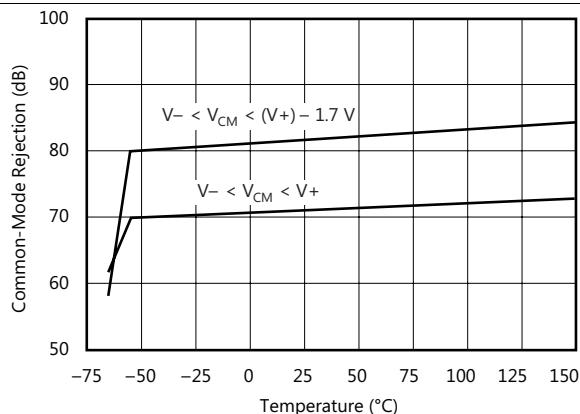


**Figure 6. Output Voltage Swing vs Output Current**

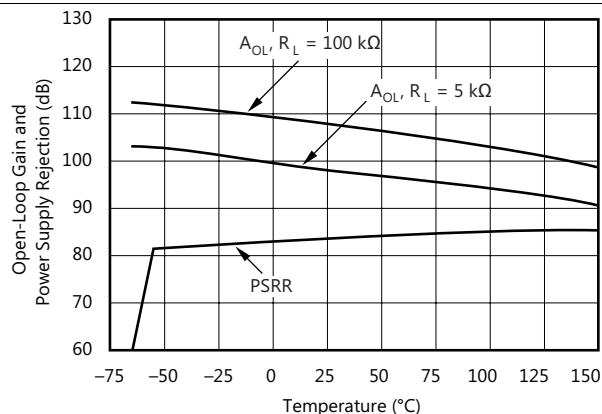


## Typical Characteristics (continued)

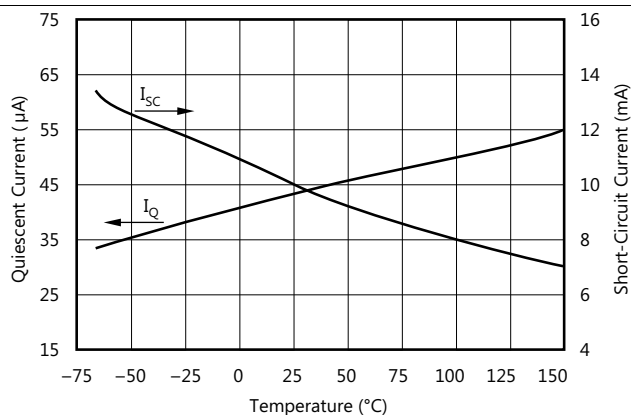
At  $T_A = 25^\circ\text{C}$ ,  $R_L = 100\text{ k}\Omega$  connected to  $V_S / 2$ ,  $V_{OUT} = V_S / 2$  (unless otherwise noted).



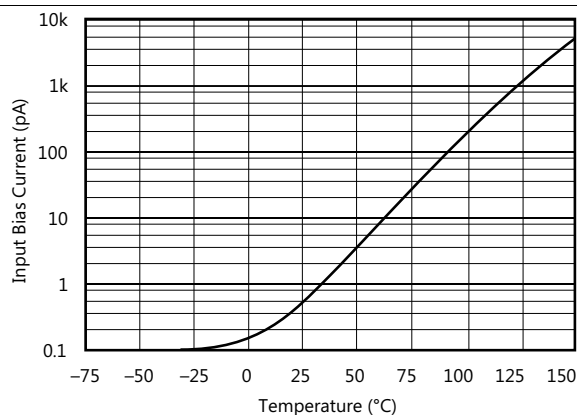
**Figure 7. Common-Mode Rejection vs Temperature**



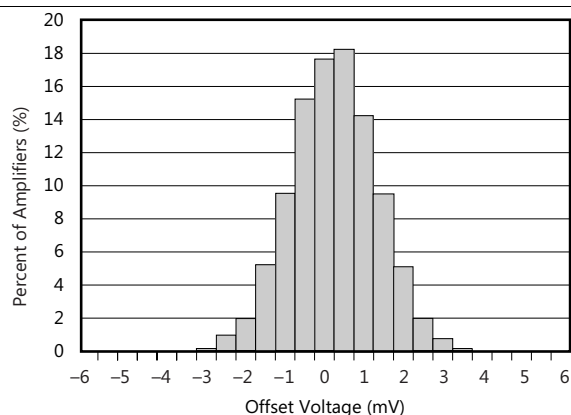
**Figure 8. Open-Loop Gain and PSRR vs Temperature**



**Figure 9. Quiescent and Short-Circuit Current vs Temperature**

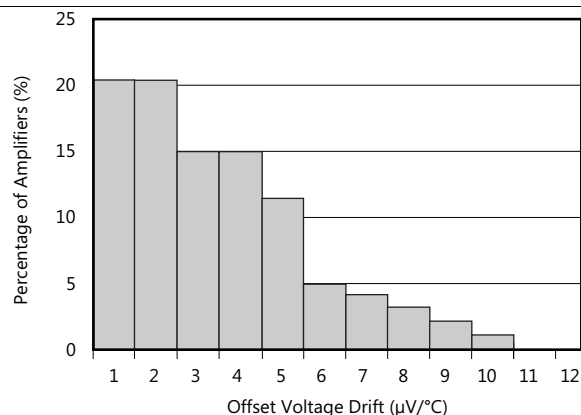


**Figure 10. Input Bias ( $I_B$ ) Current vs Temperature**



Typical production distribution of packaged units.

**Figure 11. Offset Voltage Production Distribution**

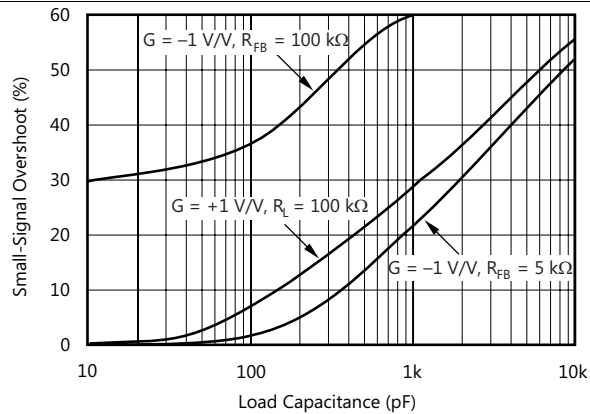


Typical production distribution of packaged units.

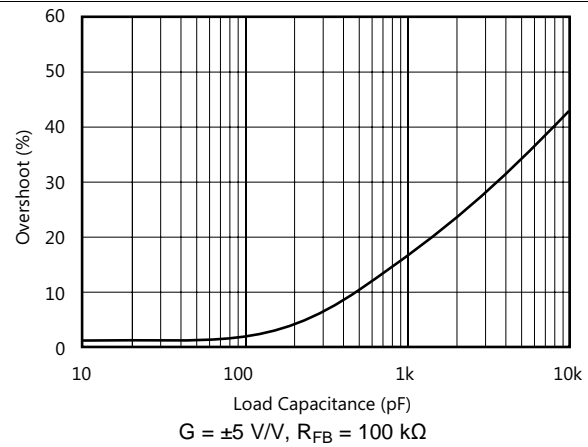
**Figure 12. Offset Voltage Drift Magnitude Production Distribution**

## Typical Characteristics (continued)

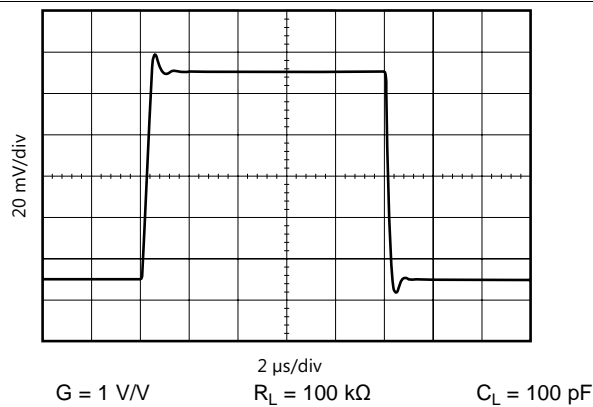
At  $T_A = 25^\circ\text{C}$ ,  $R_L = 100\text{ k}\Omega$  connected to  $V_S / 2$ ,  $V_{OUT} = V_S / 2$  (unless otherwise noted).



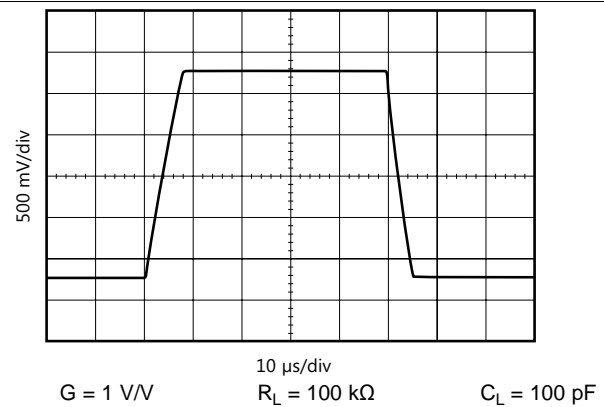
**Figure 13. Small-Signal Overshoot vs Load Capacitance**



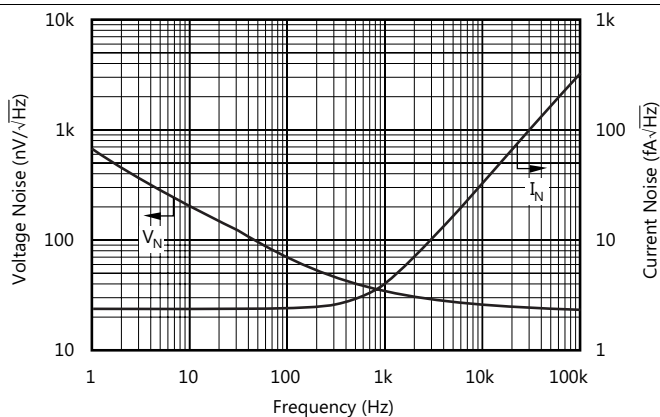
**Figure 14. Percent Overshoot vs Load Capacitance**



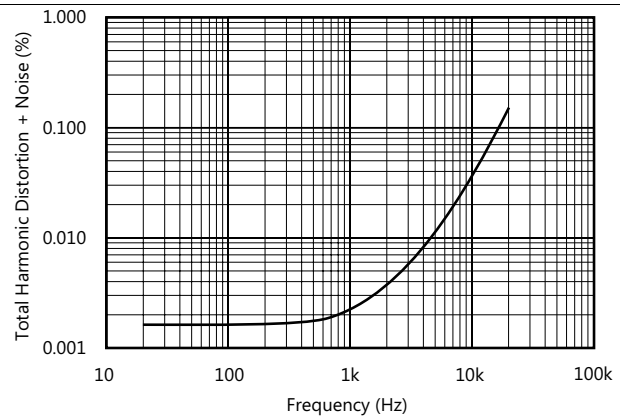
**Figure 15. Small-Signal Step Response**



**Figure 16. Large-Signal Step Response**



**Figure 17. Input Current and Voltage Noise Spectral Density vs Frequency**



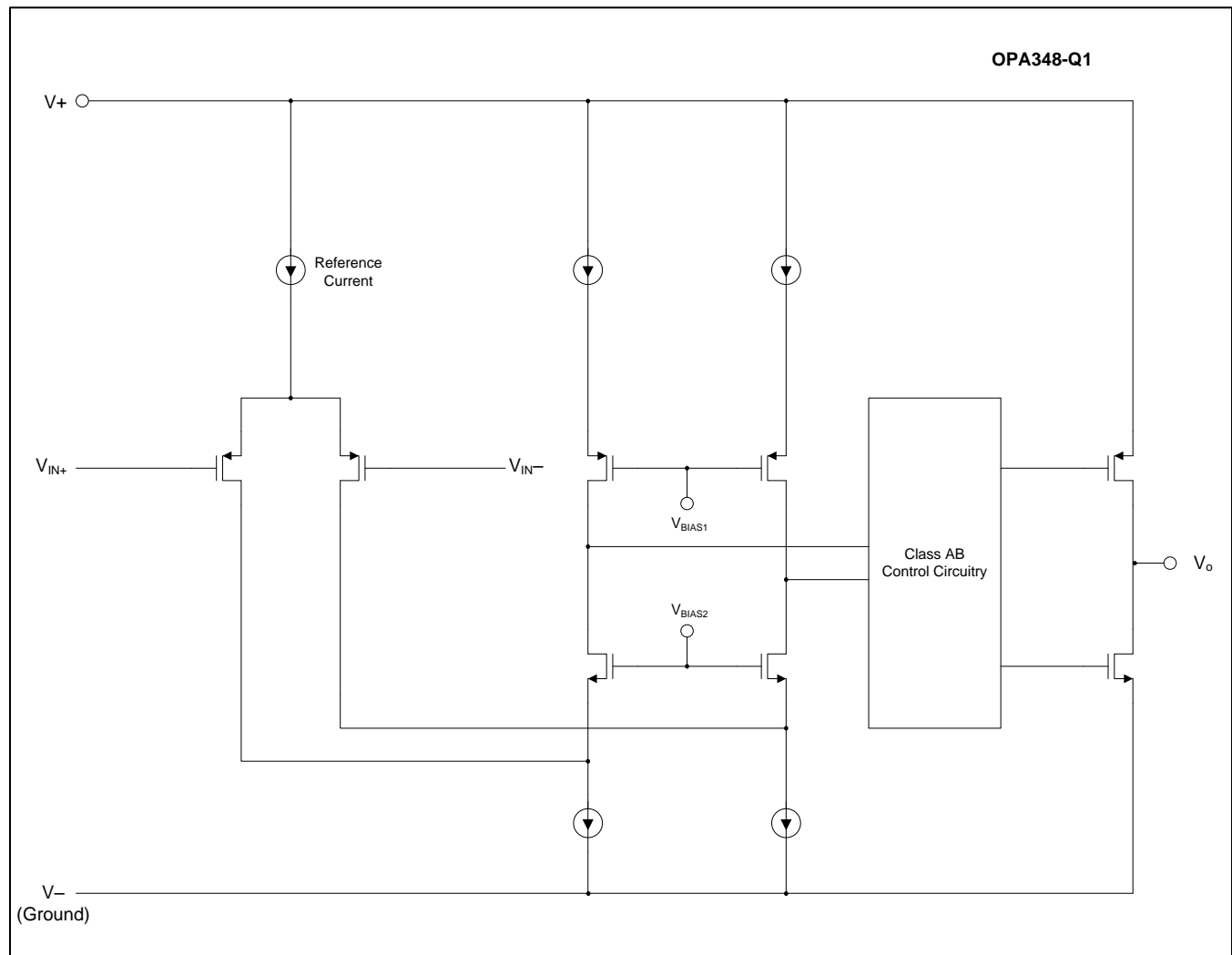
**Figure 18. Total Harmonic Distortion + Noise vs Frequency**

## 7 Detailed Description

### 7.1 Overview

The OPAx348-Q1 family of devices is a low-power, rail-to-rail input and output operational amplifier. These devices operate from 1.8 V to 5.5 V, are unity-gain stable, and are suitable for a wide range of general-purpose applications. The class AB output stage is capable of driving  $\leq 10\text{-k}\Omega$  loads connected to any point between  $V_{+}$  and ground. The input common-mode voltage range includes both rails and allows the OPAx348-Q1 family of devices to be used in virtually any single-supply application. Rail-to-rail input and output swing significantly increases dynamic range, especially in low-supply applications, and makes them ideal for driving sampling analog-to-digital converters (ADCs).

### 7.2 Functional Block Diagram



## 7.3 Feature Description

### 7.3.1 Operating Voltage

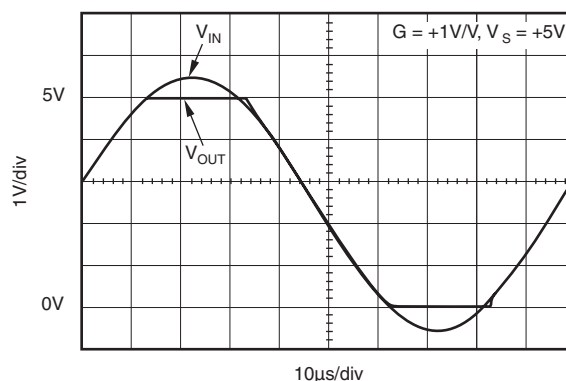
The OPAx348-Q1 op amp is fully specified and ensured for operation from 1.8 V to 5.5 V. In addition, many specifications apply from  $-40^{\circ}\text{C}$  to  $+125^{\circ}\text{C}$ . Parameters that vary significantly with operating voltages or temperature are shown in the [Typical Characteristics](#) graphs. Power-supply pins should be bypassed with 0.01- $\mu\text{F}$  ceramic capacitors.

### 7.3.2 Rail-to-Rail Input

The input common-mode voltage range of the OPAx348-Q1 family of devices extends 200 mV beyond the supply rails. This performance is achieved with a complementary input stage: an N-channel input differential pair in parallel with a P-channel differential pair. The N-channel pair is active for input voltages close to the positive rail, typically  $(V+) - 1.3\text{ V}$  to 200 mV above the positive supply. The P-channel pair is on for inputs from 200 mV below the negative supply to approximately  $(V+) - 1.3\text{ V}$ . A small transition region exists, typically  $(V+) - 1.4\text{ V}$  to  $(V+) - 1.2\text{ V}$ , in which both pairs are on. This 200-mV transition region can vary up to 300 mV with process variation. Thus, the transition region (both stages on) can range from  $(V+) - 1.7\text{ V}$  to  $(V+) - 1.5\text{ V}$  on the low end, up to  $(V+) - 1.1\text{ V}$  to  $(V+) - 0.9\text{ V}$  on the high end. Within this transition region, PSRR, CMRR, offset voltage, offset drift, and THD may be degraded compared to device operation outside this region.

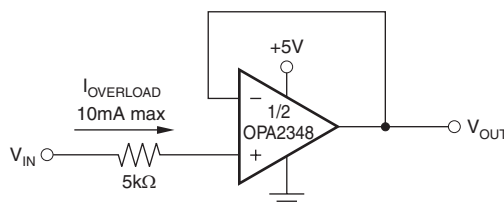
### 7.3.3 Rail-to-Rail Input

The input common-mode range extends from  $(V-) - 0.2\text{ V}$  to  $(V+) + 0.2\text{ V}$ . For normal operation, the inputs should be limited to this range. The absolute maximum input voltage is 500 mV beyond the supplies. Inputs greater than the input common-mode range but less than the maximum input voltage, while not valid, do not cause any damage to the op amp. Unlike some other op amps, if the input current is limited, the inputs may go beyond the power supplies without phase inversion, as shown in [Figure 19](#).



**Figure 19. No Phase Inversion with Inputs Greater Than Power-Supply Voltage**

Normally, input currents are 0.5 pA. However, large inputs (greater than 500 mV beyond the supply rails) can cause excessive current to flow in or out of the input pins. Therefore, limiting the input current to less than 10 mA is important as well as keeping the input voltage below the maximum rating. This limiting is easily accomplished with an input voltage resistor, as shown in [Figure 20](#).



**Figure 20. Input Current Protection for Voltages Exceeding the Supply Voltage**

## Feature Description (continued)

### 7.3.4 Input and ESD Protection

The OPAx348-Q1 family of devices incorporates internal electrostatic discharge (ESD) protection circuits on all pins. In the case of input and output pins, this protection primarily consists of current-steering diodes connected between the input and power-supply pins. These ESD protection diodes also provide in-circuit, input overdrive protection, as long as the current is limited to 10 mA as stated in the [Absolute Maximum Ratings](#) table. [Figure 21](#) shows how a series input resistor can be added to the driven input to limit the input current. The added resistor contributes thermal noise at the amplifier input and the value should be kept to a minimum in noise-sensitive applications.

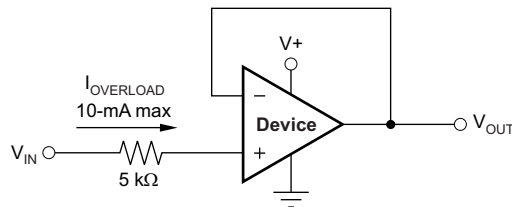


Figure 21. Input Current Protection

### 7.3.5 Common-Mode Rejection Ratio (CMRR)

CMRR for the OPAx348-Q1 family of devices is specified in several ways so the best match for a given application may be used; see the [Electrical Characteristics](#) table. First, the CMRR of the device in the common-mode range below the transition region [ $V_{CM} < (V+) - 1.3$  V] is given. This specification is the best indicator of the capability of the device when the application requires use of one of the differential input pairs. Second, the CMRR over the entire common-mode range is specified at ( $V_{CM} = -0.2$  V to 5.7 V). This last value includes the variations seen through the transition region (see [Figure 22](#)).

### 7.3.6 Common-Mode Voltage Range

The input common-mode voltage range of the OPAx348-Q1 device extends 200 mV beyond the supply rails. This extended range is achieved with a complementary input stage—an N-channel input differential pair in parallel with a P-channel differential pair. The N-channel pair is active for input voltages close to the positive rail, typically  $(V+) - 1.2$  V to 300 mV above the positive supply, while the P-channel pair is on for inputs from 300 mV below the negative supply to approximately  $(V+) - 1.4$  V. A small transition region exists, typically  $(V+) - 1.4$  V to  $(V+) - 1.2$  V, in which both pairs are on. This 200-mV transition region, shown in [Figure 22](#), can vary  $\pm 300$  mV with process variation. Thus, the transition region (both stages on) can range from  $(V+) - 1.7$  V to  $(V+) - 1.5$  V on the low end, up to  $(V+) - 1.1$  V to  $(V+) - 0.9$  V on the high end. Within the 200-mV transition region, PSRR, CMRR, offset voltage, offset drift, and THD may be degraded compared to operation outside this region.

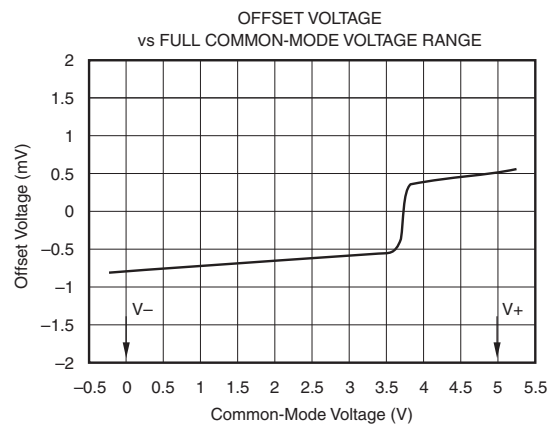


Figure 22. Behavior of Typical Transition Region at Room Temperature

## Feature Description (continued)

### 7.3.7 EMI Susceptibility and Input Filtering

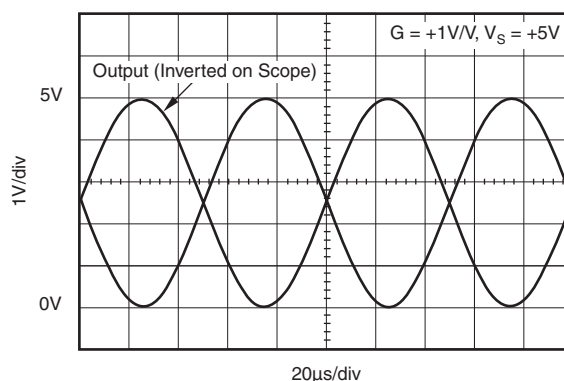
Op amps vary with regard to the susceptibility of the device to electromagnetic interference (EMI). If conducted EMI enters the op amp, the dc offset observed at the amplifier output may shift from the nominal value while EMI is present. This shift is a result of signal rectification associated with the internal semiconductor junctions. While all op amp pin functions can be affected by EMI, the signal input pins are likely to be the most susceptible. The OPAx348-Q1 family of devices incorporates an internal input, low-pass filter that reduces the amplifier response to EMI. Both common-mode and differential mode filtering are provided by this filter. The filter is designed for a cutoff frequency of approximately 80 MHz (–3 dB), with a roll-off of 20 dB per decade.

Texas Instruments has developed the ability to accurately measure and quantify the immunity of an operational amplifier over a broad frequency spectrum extending from 10 MHz to 6 GHz. The EMI rejection ratio (EMIRR) metric allows op amps to be directly compared by the EMI immunity. Detailed information can also be found in the application report, *EMI Rejection Ratio of Operational Amplifiers* (SBOA128), available for download from [www.ti.com](http://www.ti.com).

### 7.3.8 Rail-to-Rail Output

Designed as a micro-power, low-noise operational amplifier, the OPAx348-Q1 family of devices delivers a robust output drive capability. A class AB output stage with common-source transistors is used to achieve full rail-to-rail output swing capability. For resistive loads up to 10 k $\Omega$ , the output swings typically to within 5 mV of either supply rail regardless of the power-supply voltage applied. Different load conditions change the ability of the amplifier to swing close to the rails; refer to the graph, [Output Voltage Swing vs Output Current](#).

A class AB output stage with common-source transistors is used to achieve rail-to-rail output. This output stage is capable of driving 5-k $\Omega$  loads connected to any potential between V+ and ground. For light resistive loads (>100 k $\Omega$ ), the output voltage can typically swing to within 18 mV from supply rail. With moderate resistive loads (10 k $\Omega$  to 50 k $\Omega$ ), the output voltage can typically swing to within 100 mV of the supply rails while maintaining high open-loop gain (see [Figure 6](#) in the [Typical Characteristics](#) section).

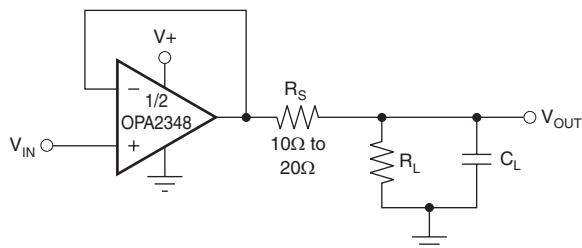


**Figure 23. Rail-to-Rail I/O**

## Feature Description (continued)

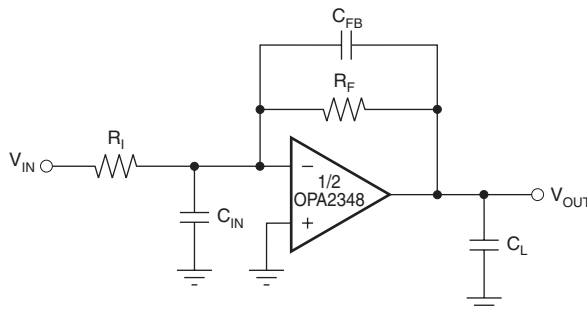
### 7.3.9 Capacitive Load and Stability

The OPAx348-Q1 family of devices in a unity-gain configuration can directly drive up to 250-pF pure capacitive load. Increasing the gain enhances the ability of the amplifier to drive greater capacitive loads (see [Figure 13](#) in the *Typical Characteristics* section). In unity-gain configurations, capacitive load drive can be improved by inserting a small ( $10\text{-}\Omega$  to  $20\text{-}\Omega$ ) resistor,  $R_S$ , in series with the output, as shown in [Figure 24](#). This resistor significantly reduces ringing while maintaining dc performance for purely capacitive loads. However, if a resistive load exists in parallel with the capacitive load, a voltage divider is created, introducing a direct current (dc) error at the output and slightly reducing the output swing. The error introduced is proportional to the ratio  $R_S/R_L$  and is generally negligible.



**Figure 24. Series Resistor in Unity-Gain Buffer Configuration Improves Capacitive Load Drive**

In unity-gain inverter configuration, the phase margin can be reduced by the reaction between the capacitance at the op amp input and the gain setting resistors, thus degrading capacitive load drive. The best performance is achieved by using small-valued resistors. For example, when driving a 500-pF load, reducing the resistor values from 100 k $\Omega$  to 5 k $\Omega$  decreases overshoot from 55% to 13% (see [Figure 13](#) in the *Typical Characteristics* section). However, when large-valued resistors cannot be avoided, a small (4-pF to 6-pF) capacitor,  $C_{FB}$ , can be inserted in the feedback loop, as shown in [Figure 25](#). This small capacitor significantly reduces overshoot by compensating the effect of capacitance,  $C_{IN}$ , which includes the input capacitance of the amplifier and printed circuit board (PCB) parasitic capacitance.



**Figure 25. Improving Capacitive Load Drive**

## 7.4 Device Functional Modes

The OPAx348-Q1 family of devices is powered on when the supply is connected. The device can be operated as a single-supply operational amplifier or a dual-supply amplifier, depending on the application.

## 8 Application and Implementation

### NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 8.1 Application Information

The OPAx348-Q1 operational amplifiers (op amps) are unity-gain stable and suitable for a wide range of general-purpose applications.

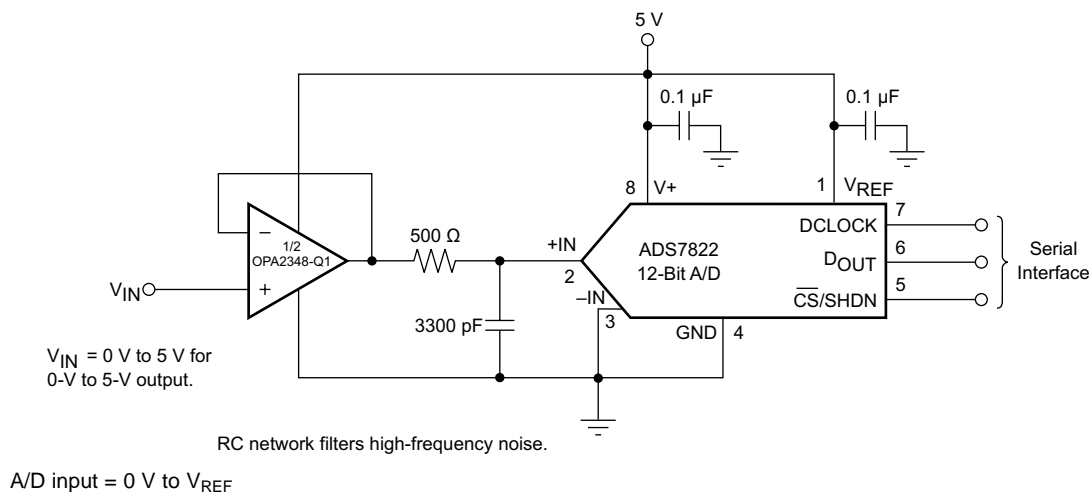
The OPAx348-Q1 device features wide bandwidth and unity-gain stability with rail-to-rail input and output for increased dynamic range. [Figure 23](#) shows the input and output waveforms for the OPAx348-Q1 device in unity-gain configuration. Operation is from a single 5-V supply with a 100-k $\Omega$  load connected to  $V_S / 2$ . The input is a 5-V<sub>PP</sub> sinusoid. Output voltage is approximately 4.98 V<sub>PP</sub>.

The power-supply pins should be bypassed with 0.01- $\mu$ F ceramic capacitors.

#### 8.1.1 Driving Analog-to-Digital Converters (ADCs)

The OPAx348-Q1 op amps are optimized for driving medium-speed sampling ADCs. The OPAx348-Q1 op amps buffer the ADC input capacitance and resulting charge injection while providing signal gain.

[Figure 26](#) shows the OPA2348 in a basic noninverting configuration driving the ADS7822 device. The ADS7822 device is a 12-bit, micropower sampling converter in the MSOP-8 package. When used with the low-power miniature packages of the OPAx348-Q1 family of devices, the combination is ideal for space-limited, low-power applications. In this configuration, an RC network at the ADC input can be used to provide for anti-aliasing filtering and charge injection current.

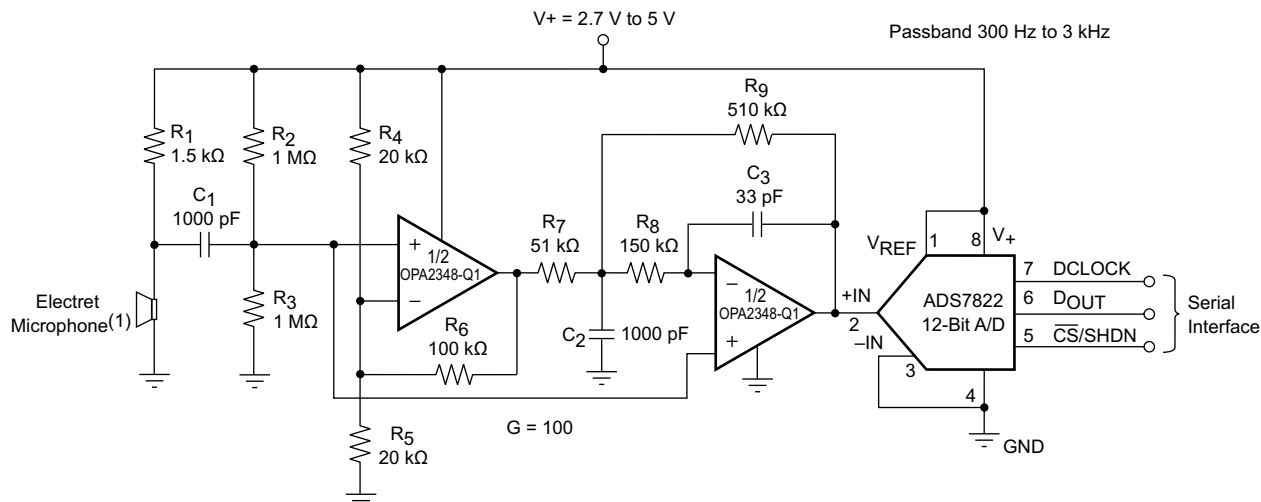


**Figure 26. Noninverting Configuration Driving ADS7822**

The OPAx348-Q1 family of devices can also be used in noninverting configuration to drive the ADS7822 device in limited low-power applications. In this configuration, an RC network at the ADC input can be used to provide for anti-aliasing filtering and charge injection current. See [Figure 26](#) for the OPAx348-Q1 driving an ADS7822 device in a speech bandpass filtered data acquisition system. This small, low-cost solution provides the necessary amplification and signal conditioning to interface directly with an electret microphone. This circuit operates with  $V_S = 2.7$  V to 5 V with less than 250- $\mu$ A typical quiescent current.



## Application Information (continued)

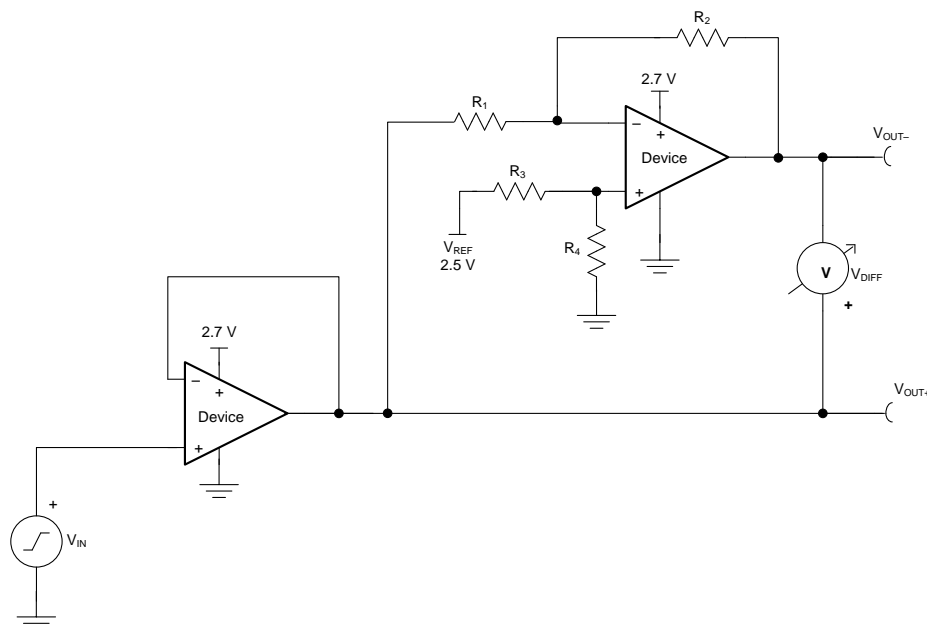


(1) Electret microphone powered by  $R_1$ .

**Figure 27. Speech Bandpass Filtered Data Acquisition System**

## 8.2 Typical Application

Some applications require differential signals. [Figure 28](#) shows a simple circuit to convert a single-ended input of 0.1 V to 2.4 V into a differential output of  $\pm 2.3$  V on a single 2.7-V supply. The output range is intentionally limited to maximize linearity. The circuit is composed of two amplifiers. One amplifier functions as a buffer and creates a voltage,  $V_{OUT+}$ . The second amplifier inverts the input and adds a reference voltage to generate  $V_{OUT-}$ . Both  $V_{OUT+}$  and  $V_{OUT-}$  range from 0.1 V to 2.4 V. The difference,  $V_{DIFF}$ , is the difference between  $V_{OUT+}$  and  $V_{OUT-}$ . This configuration makes the differential output voltage range to be 2.3 V.



**Figure 28. Schematic for a Single-Ended Input to Differential Output Conversion**

## Typical Application (continued)

### 8.2.1 Design Requirements

The design requirements are as follows:

- Supply voltage: 2.7 V
- Reference voltage: 2.5 V
- Input: 0.1 V to 2.4 V
- Output differential:  $\pm 2.3$  V
- Output common-mode voltage: 1.25 V
- Small-signal bandwidth: 1 MHz

### 8.2.2 Detailed Design Procedure

The circuit in [Figure 28](#) takes a single-ended input signal,  $V_{IN}$ , and generates two output signals,  $V_{OUT+}$  and  $V_{OUT-}$  using two amplifiers and a reference voltage,  $V_{REF}$ .  $V_{OUT+}$  is the output of the first amplifier and is a buffered version of the input signal,  $V_{IN}$  (as shown in [Equation 1](#)).  $V_{OUT-}$  is the output of the second amplifier which uses  $V_{REF}$  to add an offset voltage to  $V_{IN}$  and feedback to add inverting gain. The transfer function for  $V_{OUT-}$  is given in [Equation 2](#).

$$V_{OUT+} = V_{IN} \quad (1)$$

$$V_{OUT-} = V_{REF} \times \left( \frac{R_4}{R_3 + R_4} \right) \times \left( 1 + \frac{R_2}{R_1} \right) - V_{IN} \times \frac{R_2}{R_1} \quad (2)$$

The differential output signal,  $V_{DIFF}$ , is the difference between the two single-ended output signals,  $V_{OUT+}$  and  $V_{OUT-}$ . [Equation 3](#) shows the transfer function for  $V_{DIFF}$ . By applying the conditions that  $R_1 = R_2$  and  $R_3 = R_4$ , the transfer function is simplified into [Equation 6](#). Using this configuration, the maximum input signal is equal to the reference voltage and the maximum output of each amplifier is equal to  $V_{REF}$ . The differential output range is  $2 \times V_{REF}$ . Furthermore, the common-mode voltage ( $V_{CM}$ ) is one half of  $V_{REF}$  (see [Equation 7](#)).

$$V_{DIFF} = V_{OUT+} - V_{OUT-} = V_{IN} \times \left( 1 + \frac{R_2}{R_1} \right) - V_{REF} \times \left( \frac{R_4}{R_3 + R_4} \right) \times \left( 1 + \frac{R_2}{R_1} \right) \quad (3)$$

$$V_{OUT+} = V_{IN} \quad (4)$$

$$V_{OUT-} = V_{REF} - V_{IN} \quad (5)$$

$$V_{DIFF} = 2 \times V_{IN} - V_{REF} \quad (6)$$

$$V_{CM} = \left( \frac{V_{OUT+} + V_{OUT-}}{2} \right) = \frac{1}{2} V_{REF} \quad (7)$$

#### 8.2.2.1 Amplifier Selection

Linearity over the input range is key for good dc accuracy. The common-mode input range and output swing limitations determine the linearity. In general, an amplifier with rail-to-rail input and output swing is required. Bandwidth is a key concern for this design, so the OPAx348-Q1 family of devices is selected because its bandwidth is greater than the target of 1 MHz. The bandwidth and power ratio makes this device power-efficient, and the low offset and drift ensure good accuracy for moderate precision applications.

#### 8.2.2.2 Passive Component Selection

Because the transfer function of  $V_{OUT-}$  relies heavily upon resistors ( $R_1$ ,  $R_2$ ,  $R_3$ , and  $R_4$ ), use resistors with low tolerances to maximize performance and minimize error. This design uses resistors with resistance values of 49.9 k $\Omega$  and tolerances of 0.1%. However, if the noise of the system is a key parameter, smaller resistance values (6 k $\Omega$  or lower) can be selected to keep the overall system noise low. This technique ensures that the noise from the resistors is lower than the amplifier noise.

## Typical Application (continued)

### 8.2.3 Application Curves

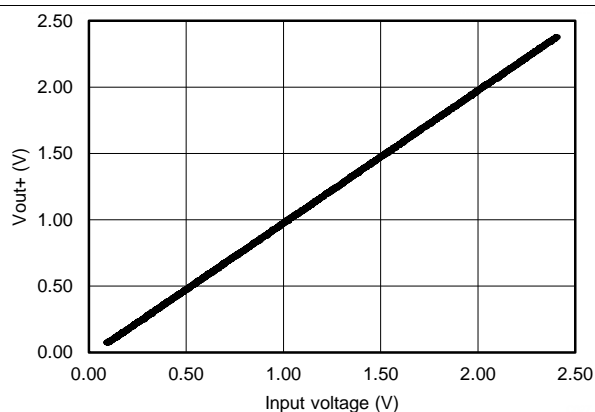


Figure 29. V<sub>OUT+</sub> vs Input Voltage

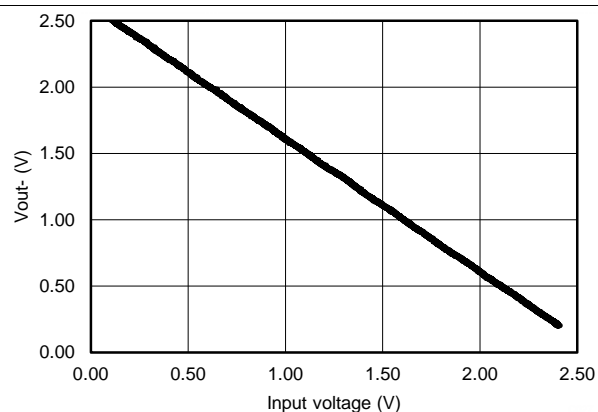


Figure 30. V<sub>OUT-</sub> vs Input Voltage

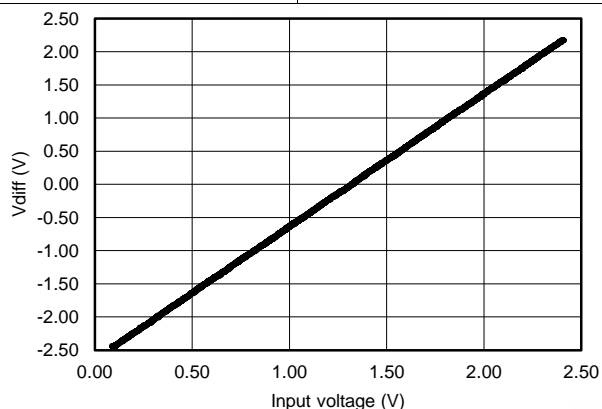


Figure 31. V<sub>DIFF</sub> vs Input Voltage

## 9 Power Supply Recommendations

The OPAx348-Q1 family of devices is specified for operation from 1.8 V to 5.5 V ( $\pm 0.9$  V to  $\pm 2.75$  V); many specifications apply from  $-40^{\circ}\text{C}$  to  $125^{\circ}\text{C}$ . The [Typical Characteristics](#) presents parameters that can exhibit significant variance with regard to operating voltage or temperature.

### CAUTION

Supply voltages larger than 7 V can permanently damage the device (see the [Absolute Maximum Ratings](#)).

Place 0.1- $\mu\text{F}$  bypass capacitors close to the power-supply pins to reduce errors coupling in from noisy or high-impedance power supplies. For more detailed information on bypass capacitor placement, refer to the [Layout Guidelines](#) section.

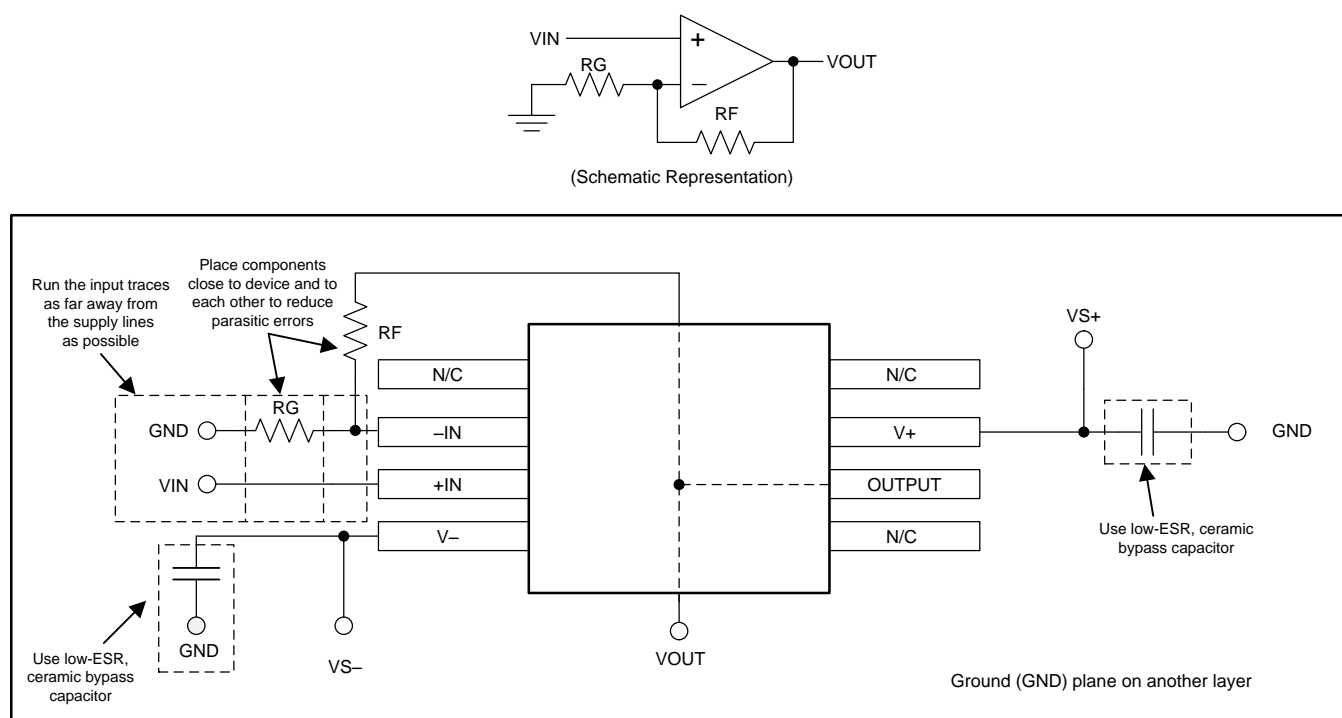
## 10 Layout

### 10.1 Layout Guidelines

For best operational performance of the device, use good PCB layout practices, including:

- Noise can propagate into analog circuitry through the power pins of the circuit as a whole and the operational amplifier. Bypass capacitors are used to reduce the coupled noise by providing low-impedance power sources local to the analog circuitry.
  - Connect low-ESR, 0.1- $\mu$ F ceramic bypass capacitors between each supply pin and ground, placed as close to the device as possible. A single bypass capacitor from V+ to ground is applicable for single-supply applications.
- Separate grounding for analog and digital portions of the circuitry is one of the simplest and most effective methods of noise suppression. One or more layers on multilayer PCBs are usually devoted to ground planes. A ground plane helps distribute heat and reduces EMI noise pickup. Make sure to physically separate digital and analog grounds, paying attention to the flow of the ground current. For more detailed information, refer to *Circuit Board Layout Techniques*, [SLOA089](#).
- To reduce parasitic coupling, run the input traces as far away from the supply or output traces as possible. If these traces cannot be kept separate, crossing the sensitive trace perpendicularly is much better than crossing in parallel with the noisy trace.
- Place the external components as close to the device as possible. Keep RF and RG close to the inverting input to minimize parasitic capacitance, as shown in [Figure 32](#).
- Keep the length of input traces as short as possible. Always remember that the input traces are the most sensitive part of the circuit.
- Consider a driven, low-impedance guard ring around the critical traces. A guard ring can significantly reduce leakage currents from nearby traces that are at different potentials.

### 10.2 Layout Example



**Figure 32. Operational Amplifier Board Layout for Noninverting Configuration**

## 11 Device and Documentation Support

### 11.1 Documentation Support

#### 11.1.1 Related Documentation

For related documentation see the following:

- ADS7822: 12-Bit, 200kHz, microPower Sampling Analog-to-Digital Converter, [SBAS062](#)
- Application report: *Circuit Board Layout Techniques*, [SLOA089](#)
- Application report: *EMI Rejection Ratio of Operational Amplifiers*, [SBOA128](#)

### 11.2 Related Links

[Table 1](#) lists quick access links. Categories include technical documents, support and community resources, tools and software, and quick access to sample or buy.

**Table 1. Related Links**

PARTS	PRODUCT FOLDER	SAMPLE & BUY	TECHNICAL DOCUMENTS	TOOLS & SOFTWARE	SUPPORT & COMMUNITY
OPA348-Q1	<a href="#">Click here</a>	<a href="#">Click here</a>	<a href="#">Click here</a>	<a href="#">Click here</a>	<a href="#">Click here</a>
OPA2348-Q1	<a href="#">Click here</a>	<a href="#">Click here</a>	<a href="#">Click here</a>	<a href="#">Click here</a>	<a href="#">Click here</a>
OPA4348-Q1	<a href="#">Click here</a>	<a href="#">Click here</a>	<a href="#">Click here</a>	<a href="#">Click here</a>	<a href="#">Click here</a>

### 11.3 Community Resource

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

**TI E2E™ Online Community** *TI's Engineer-to-Engineer (E2E) Community*. Created to foster collaboration among engineers. At [e2e.ti.com](#), you can ask questions, share knowledge, explore ideas and help solve problems with fellow engineers.

**Design Support** *TI's Design Support* Quickly find helpful E2E forums along with design support tools and contact information for technical support.

### 11.4 Trademarks

E2E is a trademark of Texas Instruments.

All other trademarks are the property of their respective owners.

### 11.5 Electrostatic Discharge Caution



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

### 11.6 Glossary

[SLYZ022](#) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

## 12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

## PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead/Ball Finish (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
OPA2348AQDRQ1	ACTIVE	SOIC	D	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	-40 to 125	OPA 2348Q	<a href="#">Samples</a>
OPA348AQDBVRQ1	ACTIVE	SOT-23	DBV	5	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	-40 to 125	A48	<a href="#">Samples</a>
OPA348AQDRQ1	ACTIVE	SOIC	D	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	-40 to 125	348Q1	<a href="#">Samples</a>
OPA4348AQPWRQ1	ACTIVE	TSSOP	PW	14	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-3-260C-168 HR	-40 to 125	OP4348Q	<a href="#">Samples</a>

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

**Green (RoHS & no Sb/Br):** TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

**Important Information and Disclaimer:** The information provided on this page represents TI's knowledge and belief as of the date that it is provided. TI bases its knowledge and belief on information provided by third parties, and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. TI has taken and continues to take reasonable steps to provide representative and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. TI and TI suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.

In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

**OTHER QUALIFIED VERSIONS OF OPA2348-Q1, OPA348-Q1, OPA4348-Q1 :**

- Catalog: [OPA2348](#), [OPA348](#), [OPA4348](#)

NOTE: Qualified Version Definitions:

- Catalog - TI's standard catalog product

**TAPE AND REEL INFORMATION**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
OPA2348AQDRQ1	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
OPA348AQDBVRQ1	SOT-23	DBV	5	3000	178.0	9.0	3.3	3.2	1.4	4.0	8.0	Q3
OPA348AQDRQ1	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
OPA4348AQPWRQ1	TSSOP	PW	14	2500	330.0	12.4	6.9	5.6	1.6	8.0	12.0	Q1



## TAPE AND REEL BOX DIMENSIONS



\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
OPA2348AQDRQ1	SOIC	D	8	2500	367.0	367.0	35.0
OPA348AQDBVRQ1	SOT-23	DBV	5	3000	180.0	180.0	18.0
OPA348AQDRQ1	SOIC	D	8	2500	367.0	367.0	35.0
OPA4348AQPWRQ1	TSSOP	PW	14	2500	367.0	367.0	35.0

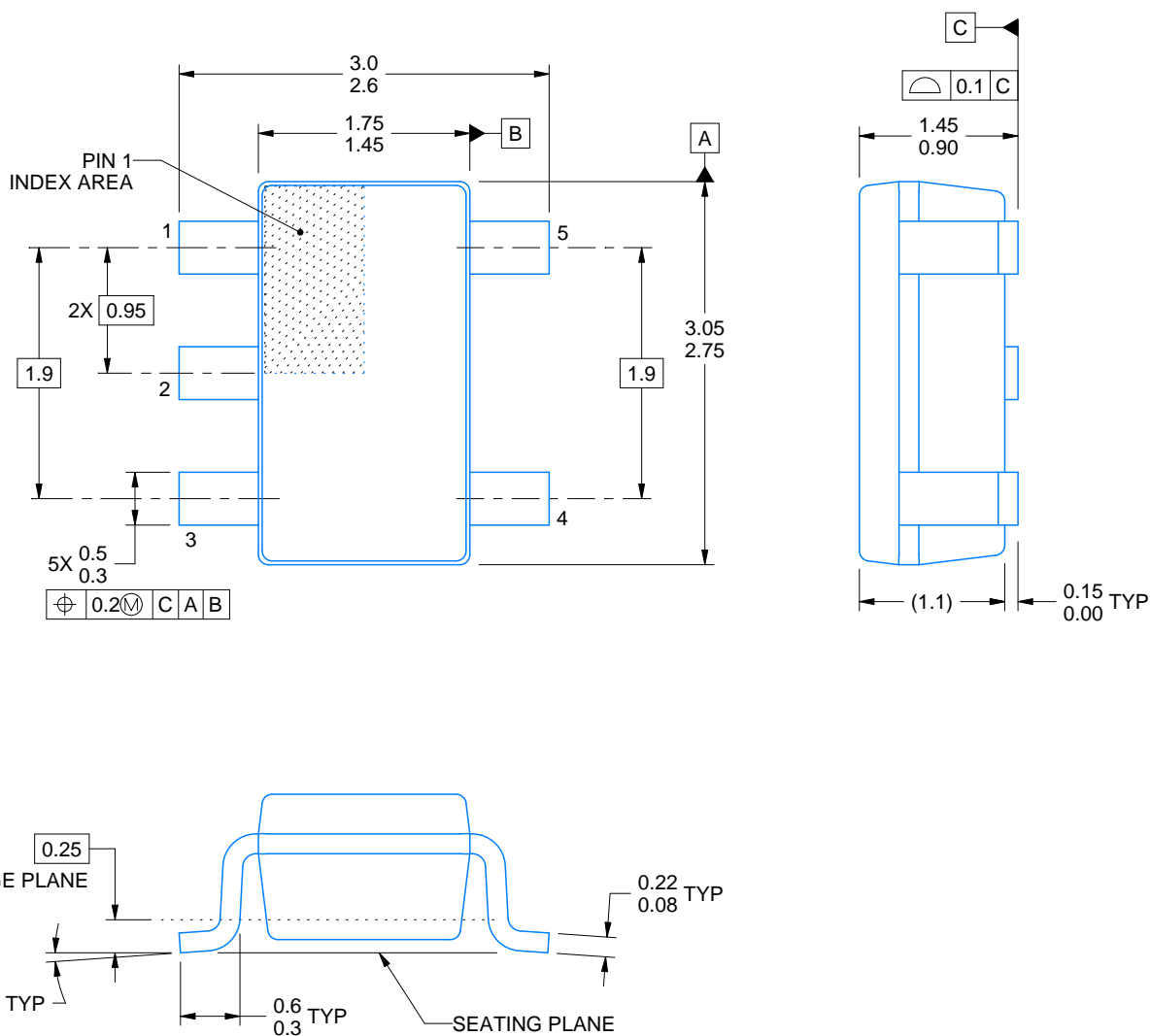


**DBV0005A**

# PACKAGE OUTLINE

**SOT-23 - 1.45 mm max height**

SMALL OUTLINE TRANSISTOR



4214839/E 09/2019

## NOTES:

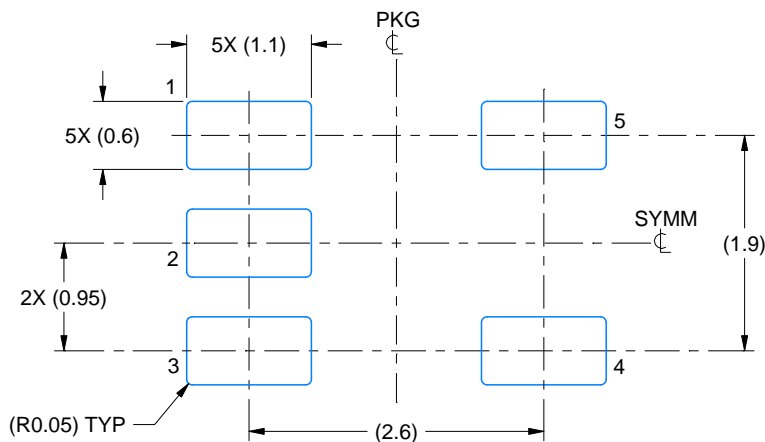
1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. Reference JEDEC MO-178.
4. Body dimensions do not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.

# EXAMPLE BOARD LAYOUT

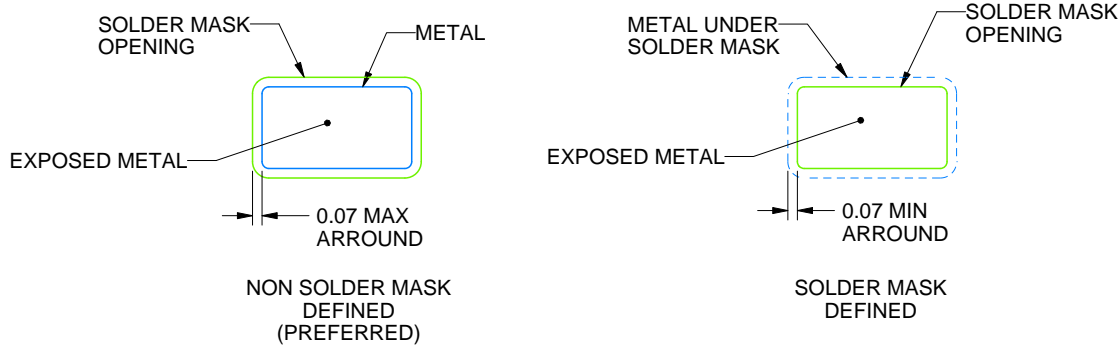
DBV0005A

SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:15X



SOLDER MASK DETAILS

4214839/E 09/2019

NOTES: (continued)

5. Publication IPC-7351 may have alternate designs.
6. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

## EXAMPLE STENCIL DESIGN

DBV0005A

SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR



SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL  
SCALE:15X

4214839/E 09/2019

NOTES: (continued)

7. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
8. Board assembly site may have different recommendations for stencil design.

PW (R-PDSO-G14)

PLASTIC SMALL OUTLINE



4040064-3/G 02/11

- NOTES:
- A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.
  - B. This drawing is subject to change without notice.
  - C. Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0,15 each side.
  - D. Body width does not include interlead flash. Interlead flash shall not exceed 0,25 each side.
  - E. Falls within JEDEC MO-153

PW (R-PDSO-G14)

PLASTIC SMALL OUTLINE



- NOTES:
- A. All linear dimensions are in millimeters.
  - B. This drawing is subject to change without notice.
  - C. Publication IPC-7351 is recommended for alternate designs.
  - D. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC-7525 for other stencil recommendations.
  - E. Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.



**D0008A**

# PACKAGE OUTLINE

**SOIC - 1.75 mm max height**

SMALL OUTLINE INTEGRATED CIRCUIT



## NOTES:

1. Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed .006 [0.15] per side.
4. This dimension does not include interlead flash.
5. Reference JEDEC registration MS-012, variation AA.

# EXAMPLE BOARD LAYOUT

D0008A

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:8X



SOLDER MASK DETAILS

4214825/C 02/2019

NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



## EXAMPLE STENCIL DESIGN

D0008A

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



SOLDER PASTE EXAMPLE  
BASED ON .005 INCH [0.125 MM] THICK STENCIL  
SCALE:8X

4214825/C 02/2019

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.

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